and, by (14)

$$\hat{U}(s) = \begin{pmatrix} se^{-sh} & -1\\ 1 & 0 \end{pmatrix}, \qquad \hat{X}(s) = \begin{pmatrix} 0 & 0\\ e^{-sh} - 1 & 0 \end{pmatrix}$$

Starting, e.g., from zero initial conditions except for  $x(0) = (x_{10}, x_{20})^T$  we get the Laplace transforms of the distributional control and trajectory

$$\hat{u}(s) = ((se^{-sh} - s)x_{10} - x_{20}, x_{10})^T, \quad \hat{x}(s) = (0, (e^{-sh} - 1)x_{10})^T.$$

To get regular controls we use Procedure 2. Solving (16) we obtain (nonuniquely)

$$\overline{U}_{1} = \begin{pmatrix} c^{2}(d-1) & -2cd(d-1) \\ -c^{2} & 2cd \end{pmatrix},$$
  
$$\overline{U}_{2} = \begin{pmatrix} c^{3}(d-1) & -2c^{2}d(d-1) - c^{2} \\ -c^{2}(c+1) & 2c(c+1)d \end{pmatrix}$$

Choose  $c_1 = 0$ ,  $c_2 = 1$ . Hence,  $U^1 = 0$ ,  $X^1 = \theta_0(1 - d)I + \theta_0^2 A$  and

$$U^{2} = \theta_{1} \begin{pmatrix} (e^{-h} - d + \theta_{1})(d - 1) & -2d(d - 1)(e^{-h} - d + \theta_{1}) - \theta_{1} \\ -e^{-h} + d - 2\theta_{1} & 2d(e^{-h} - d + 2\theta_{1}) \end{pmatrix},$$
  
$$X^{2} = \theta_{1} \begin{pmatrix} e^{-h} - d - \theta_{1}(d^{2} + 1) & \theta_{1}(2d^{3} + d + 1) \\ \theta_{1}(d - 1) & \theta_{1}(-2d^{2} + 2d - 1) + e^{-h} - d \end{pmatrix}.$$

Next, we solve (21), which takes the form

$$q_1(1-d)^2 + q_2(e^{-h}-d)^2 = 1$$

obtaining the following solution (of minimal degree)

$$q_1 = (e^{-h} - 1)^{-3}(-2d + 3e^{-h} - 1), \quad q_2 = (e^{-h} - 1)^{-3}(2d + e^{-h} - 3).$$

Performing Steps 5-7 we get formulas for Laplace transforms of regular control and trajectory corresponding to given initial conditions. For instance, if  $\Phi = 0$ ,  $\Psi = 0$ , and  $x(0) = [1, 1]^T$ , the control is given by  $\hat{u}(s) = [\hat{u}_1(s), \hat{u}_2(s)]^T$ 

$$\hat{u}_{1}(s) = (e^{-h} - 1)^{-3}(2e^{-sh} + e^{-h} - 3)\hat{\theta}_{1}(s)$$

$$\cdot \left[ (e^{-sh} - 1)(e^{-h} - e^{-sh})(1 - 2e^{-2sh}) + \hat{\theta}_{1}(s)(-2 + 3e^{-sh} - 2e^{-2sh}) \right]$$

$$\hat{u}_{2}(s) = (e^{-h} - 1)^{-3}(2e^{-sh} + e^{-h} - 3)\hat{\theta}_{1}(s)$$

$$\cdot (e^{-h} - e^{-sh} + 2\hat{\theta}_{1}(s)(-1 + 2e^{-sh}))$$

where

 $\hat{\theta}_1(s) = (e^{-h} - e^{-sh})(s-1)^{-1}$ 

The Laplace transform  $\hat{x}(s) = [\hat{x}_1(s), \hat{x}_2(s)]^T$  of the state trajectory is

$$\begin{aligned} \hat{x}_1(s) &= \hat{q}_1(s)\hat{\theta}_0(s)(1 - e^{-sh} + \hat{\theta}_0(s) + \hat{\theta}_0(s)e^{-sh}) \\ &+ \hat{q}_2(s)\hat{\theta}_1(s)(e^{-h} - e^{-sh} + \hat{\theta}_1(s)(e^{-sh} - e^{-2sh} + 2e^{-3sh})) \\ \hat{x}_2(s) &= \hat{q}_1(s)\hat{\theta}_0(s)(1 - e^{-sh}) \\ &+ \hat{q}_2(s)\hat{\theta}_1(s)(e^{-h} - e^{-sh} + \hat{\theta}_1(s)(-2 + 3e^{-sh} - 2e^{-2sh})) \end{aligned}$$

where

$$q_1(s) = (e^{-h} - 1)^{-3}(-2e^{-sh} + 3e^{-h} - 1),$$
  
$$q_2(s) = (e^{-h} - 1)^{-3}(2e^{-sh} + e^{-h} - 3),$$

$$\hat{\theta}_0(s) = (1 - e^{-sh})s^{-1}.$$

## **IV.** CONCLUSIONS

Under the assumption of reachability over the polynomial ring  $\mathbb{R}[d]$  of the matrix pair characterizing a linear system with commensurate delays it has been shown that the system can be controlled to the origin and stay there while the control also vanishes identically after some time. This means that the full state of the system becomes zero identically after some finite time. Two constructive procedures have been presented which allow us to calculate easily Laplace transforms of the control and state trajectory.

### REFERENCES

- H. T. Banks, M. Q. Jacobs, and C. E. Langenhop, "Characterization of the controlled states in W<sup>(1)</sup><sub>2</sub> of linear hereditary systems," SIAM J. Contr., vol. 13, no. 3, pp. 611-649, 1975.
- [2] E. B. Lee and A. W. Olbrot, "On reachability of polynomial rings and a related genericity problem," *Int. J. Syst. Sci.*, to be published.
- genericity problem," Int. J. Syst. Sci., to be published.
  [3] A. W. Olbrot, "Genericity and nongenericity of mathematical model properties," Archiv. Autom. Telemech., vol. XXV, no. 4, pp. 473-481, 1980.
  [4] —, "Algebraic criteria of controllability to zero function for linear constant time-lag systems," Contr. Cybern., vol. 2, pp. 59-77, 1973.
  [5] A. W. Olbrot and S. H. Zak, "Controllability and observability problems for linear functional-differential systems," Found. Contr. Eng., vol. 5, no. 2, pp. 79-89, 1980.

# **On Model Reduction by Modified Cauer Form**

## R. PARTHASARATHY, K. N. JAYASIMHA, AND SARASU JOHN

Abstract - A simple algorithm for obtaining the continued fraction quotients in the modified Cauer form (MCF) from the given system matrices in companion form is presented. In the sequel, the triple of all lower order models in companion form is directly obtained. A matrix method of obtaining the time-moments and Markov parameters from the MCF quotients is also outlined. Finally, it is shown that system reduction by matching a set of MCF quotients is equivalent to system reduction by matching a set of time-moments and Markov parameters.

## I. INTRODUCTION

The problem considered by Khatwani et al. [1] is how to obtain the scalar quotients  $h_1, k_1, h_2, k_2, \cdots$  in the following modified Cauer form (MCF) representation:

$$g(s) = \frac{1}{h_1 + \frac{s}{k_1 + \frac{1}{h_2 + \frac{s}{k_2 + \frac{1}{1}}}}}$$
(1)

given the system matrices (A, B, C) in companion form. Chuang [9] modified the continued fraction technique for model reduction into this form to overcome instability.

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The procedure proposed in [1] requires the construction of a large array, the computation of whose elements involves first the evaluation of higher powers of A and  $A^{-1}$  and then the matrix products  $CA^{k}B$ ,  $k = 0, 1, 2, \cdots$ , and  $CA^{-k}B$ ,  $k = 1, 2, \cdots$ .

In this paper, we first formulate a Routh-type array which is simple to construct. We then evaluate the scalar quotients of MCF and use them to develop an inversion table from which the triple of all lower order models in companion form is directly read off. A matrix method to obtain the time-moments and Markov parameters of the system is also presented. Finally, we prove that the method of model simplification via the MCF is equivalent to model reduction by matching the first k time-moments and first k Markov parameters corresponding to the kth order of the reduced model. In this respect, the result for the second Cauer form is available in [7], [8].

# II. DEVELOPMENT OF THE ALGORITHM

Given the system matrices in companion form, viz.

$$A = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & 0 & \cdots & 1 \\ -a_{1,1} & -a_{1,2} & -a_{1,3} & \cdots & -a_{1,n} \end{bmatrix}$$
$$B = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}, \quad C = [b_{1,1}b_{1,2}b_{1,3}\cdots b_{1,n}]. \quad (2)$$

The transfer function can straightaway be written as

$$g(s) = \frac{b_{1,1} + b_{1,2}s + b_{1,3}s^2 + \dots + b_{1,n}s^{n-1}}{a_{1,1} + a_{1,2} + a_{1,3}s^2 + \dots + a_{1,n}s^{n-1} + s^n}$$
(3)

from which, using algorithm [3], we evaluate the MCF quotients by formulating the modified Routh array as follows:

$$h_{1} = \frac{a_{1,1}}{b_{1,1}} \begin{pmatrix} a_{1,1} & a_{1,2} & \cdots & a_{1,n-1} & a_{1,n} & \mathbf{1} \\ b_{1,1} & b_{1,2} & \cdots & b_{1,n-1} & b_{1,n} \\ a_{2,1} & a_{2,2} & \cdots & a_{2,n-1} & \mathbf{1} \end{pmatrix} k_{1} = b_{1,n} \\ \vdots & \vdots \\ a_{n,1} & \mathbf{1} \\ h_{n} = \frac{a_{n,1}}{b_{n,1}} \begin{pmatrix} a_{1,1} & a_{1,2} & \cdots & a_{1,n-1} & a_{1,n} & \mathbf{1} \\ \vdots & \vdots \\ a_{n,1} & \mathbf{1} & a_{n,1} & \mathbf{1} \\ b_{n,1} & b_{n,1} & b_{n,1} \end{pmatrix} k_{n} = b_{n,1}.$$
(4)

Once the MCF quotients are evaluated, we formulate the inversion table [4]:

The first two rows are built out of the elements  $p_{1,1} = h_1$ ,  $q_{1,1} = h_1 k_1$ ,

 $q_{1,2} = 1$ ,  $l_{1,1} = 1$ , and  $r_{1,1} = k_1$ . The subsequent rows are evaluated for  $i = 2, 3, \dots, n$  by the recursive relations

$$p_{i,j} = p_{i-1,j} + q_{i-1,j}h_i, \qquad j = 1, 2, \cdots, i q_{i,j} = q_{i-1,j-1} + p_{i,j}k_i, \qquad j = 1, 2, \cdots, i + 1 l_{i,j} = l_{i-1,j} + r_{i-1,j}h_i, \qquad j = 1, 2, \cdots, i - 1 r_{i,j} = r_{i-1,j-1} + l_{i,j}k_i, \qquad j = 1, 2, \cdots, i$$
 (6)

with  $q_{i,0} = 0$  and  $r_{i,0} = 0$ .

#### Lower Order Canonical Realizations

These are obtained in the form defined in (2), by reading off from (5) the values  $a_{1,1}, a_{1,2}, \cdots$  and  $b_{1,1}, b_{1,2}, \cdots$  as per the relations

$$a_{1,i} = q_{k,i}$$
  

$$b_{1,i} = r_{k,i}$$
  

$$k = 2, 3, \cdots, n-1, i = 1, 2, \cdots, k.$$
(7)

#### Evaluation of Time Moments and Markov Parameters

From the entries of the inversion table in (5), the weighted timemoments  $C_i$  (viz.  $C_i = \langle (-1)^i / (i!) \rangle m_i$ , where  $m_i$  is the *i*th time-moment of the system) and Markov parameters  $D_i$  are determined by the following matrix relations [2]:

$$\begin{bmatrix} q_{1,1} & & & \\ q_{2,2} & q_{2,1} & & \\ q_{3,3} & q_{3,2} & q_{3,1} \\ \vdots & \vdots & \vdots & \ddots \\ q_{n,n} & q_{n,n-1} & q_{n,n-2} & \cdots & q_{n,1} \end{bmatrix} \begin{bmatrix} C_0 \\ C_1 \\ C_2 \\ \vdots \\ C_{n-1} \end{bmatrix} = \begin{bmatrix} r_{1,1} \\ r_{2,2} \\ r_{3,3} \\ \vdots \\ r_{n,n} \end{bmatrix}$$
(8)

and

$$\begin{bmatrix} 1 & & & & \\ q_{2,2} & 1 & & & \\ q_{3,2} & q_{3,3} & 1 & & \\ \vdots & \vdots & \vdots & \ddots & \\ q_{n,2} & q_{n,3} & q_{n,4} & \cdots & 1 \end{bmatrix} \begin{bmatrix} D_1 \\ D_2 \\ D_3 \\ \vdots \\ D_n \end{bmatrix} = \begin{bmatrix} r_{1,1} \\ r_{2,1} \\ r_{3,1} \\ \vdots \\ r_{n,1} \end{bmatrix}.$$
(9)

The Q-matrices composed of  $q_{i,j}$  elements as shown in (8) and (9) are formed, respectively, out of the elements in (5) as defined by

$$q_{i,i-j}, \quad i = 1, 2, \cdots, n, j = 0, 1, \cdots, i-1$$
$$q_{i,j}, \quad i = 1, 2, \cdots, n, j = 2, 3, \cdots, i+1.$$
(10)

## III. Equivalence of the MCF Technique with Mixed Method

In the MCF approach to system reduction, the model parameters for the lower order model are obtained by solving the set of equations

$$\begin{aligned} h'_i &= h_i \\ k'_i &= k_i \end{aligned} \qquad i = 1, 2, \cdots$$
 (11)

while in the mixed method [5], the model parameters are obtained by solving the equations

$$C'_i = C_i, \qquad i = 0, 1, 2, \cdots$$
  
 $D'_i = D_i, \qquad i = 1, 2, \cdots$ 
(12)

We now prove that matching in (11) is equivalent to matching in (12). *Proof:* From the recursive relations in (6), we observe that

$$r_{1,1} = r_{2,2} = r_{3,3} = \dots = r_{n,n} = k_1.$$
 (13)

From (6), (8), and (9),  $h_1 = q_1$ ,  $1/k_1$ ,  $C_0 = r_{1,1}/q_{1,1} = k_1/q_{1,1}$ , and  $D_1 = r_{1,1}$ . Thus,  $h_1 = 1/C_0$  and  $k_1 = D_1$ . Matching  $h'_1 = h_1$  and  $k'_1 = k_1$ , we

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obtain

$$C'_0 = C_0 \text{ and } D'_1 = D_1.$$
 (14)

From (8),  $q_{2,2}C_0 + q_{2,1}C_1 = r_{2,2}$ . Substituting for  $q_{2,2}, q_{2,1}, r_{2,2}$ , and  $C_0$ from (6) and (13) we get

$$(h_1k_1 + h_2k_2) \cdot (1/h_1) + (h_1k_2 + h_1k_1h_2k_2)C_1 = k_1$$

which gives

$$h_2 = -(h_1^2 C_1 k_2) / (k_2 + h_1^2 k_1 k_2 C_1) = -(C_1) / (C_0^2 + C_1 D_1).$$
(15)

Similarly, from  $D_1q_{2,2} + D_2 = r_{2,1}$  [see (9)] we obtain

$$k_2 = \left( D_1^2 + C_0 D_2 \right) / C_0. \tag{16}$$

Matching  $h'_2 = h_2$  and  $k'_2 = k_2$  leads to

$$\frac{C_1'}{C_0'^2 + C_1'D_1'} = \frac{C_1}{C_0^2 + C_1D_1}$$

and

$$\frac{D_1'^2 + C_0' D_2'}{C_0'} = \frac{D_1^2 + C_0 D_2}{C_0}.$$

Since  $C'_0 = C_0$  and  $D'_1 = D_1$ , it follows that

$$C_1' = C_1, \quad D_2' = D_2 \tag{17}$$

and so on.

## IV. EXAMPLE

Consider the same example treated earlier in [1] for which lower order models are required:

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -90 & -60 & -24 & -5 \end{bmatrix},$$
$$B = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \\ 1 \end{bmatrix}, \quad C = \begin{bmatrix} 15 & 5 & 1 & 1/6 \end{bmatrix}. \tag{18}$$

The corresponding transfer function is

$$g(s) = \frac{15+5s+s^2+(1/6)s^3}{90+60s+24s^2+5s^3+s^4}.$$
 (19)

MCF Quotients: By forming the table in (4), we obtain

$$h_1 = 6, k_1 = 1/6, h_2 = 3, k_2 = 1/3, h_3 = 2, k_3 = 1,$$
  
 $h_4 = 1/5, \text{ and } k_4 = 5.$  (20)

The inversion table is as follows

Lower Order Models: From (7),

$$a_{3} = (-a_{1,1} - a_{1,2} - a_{1,3}) = (-15 - 10 - 4)$$

$$c_{3} = [b_{1,1} \ b_{1,2} \ b_{1,3}] = [5/2 \ 5/6 \ 1/6]$$

$$a_{2} = (-a_{1,1} - a_{1,2}) = (-3, -2),$$

$$c_{2} = [b_{1,1} \ b_{1,2}] = [1/2 \ 1/6].$$
(22)

Weighted Time - Moments and Markov Parameters: From (8) and (9),

$$C_0 = 1/6, C_1 = -1/18, C_2 = 1/270, C_3 = 2/405$$
  
 $D_1 = 1/6, D_2 = 1/6, D_3 = 1/6, D_4 = 1/6.$  (23)

### V. CONCLUSION

A computationally efficient procedure which involves constructing only a simple modified Routh array is presented to evaluate the continued fraction quotients from the given system matrices in companion form. The saving in computation over the earlier method of Khatwani et al. [1] is obvious: the proposed method does not require any matrix inversion or multiplication of the system matrices. The canonical realizations of all lower order models are directly read off from the inversion table.

A matrix method is presented to determine the time moments and Markov parameters from the knowledge of the MCF quotients. Furthermore, it is shown that system reduction by MCF is equivalent to system reduction by matching a set of time-moments and Markov parameters. These results find application in many practical problems, as the canonical realization possesses distinct advantages for simulation studies and for system design [6].

The steps in the algorithm are oriented for easy and direct programming. The relationship between the original state vector and the state vector of the model obtained through MCF quotients has been investigated and has been reported elsewhere [3].

### REFERENCES

- [1] K. J. Khatwani, R. K. Tiwari, and J. S. Bajwa, "On Chuang's continued-fraction method of system reduction," IEEE Trans. Automat. Contr., vol. AC-25, pp. 822-824, Aug. 1980.
- S. John, "System reduction using modified Cauer continued fraction and its applica-tion to suboptimal control," Ph.D. dissertation, Indian Inst. Technol., Madras, India, [2] Oct. 1980.
- [3] R. Parthasarathy and S. John, "State-space models using modified Cauer continued fraction," Proc. IEEE, vol. 70, pp. 300-301, Mar. 1982.
- [4] , Model generation with modified Cauer continued fraction," Arch. Elek. Ubertragung, vol. 33, pp. 289–292, July-Aug. 1979.
  [5] R. Parthasarathy and H. Singh, "A mixed method for simplification of large system dynamics," Proc. IEEE, vol. 65, pp. 1604–1605, Nov. 1977.
  [6] P. D. B. "Constraints and the state of the system of the system
- [6] R. Parthasarathy, "On canonic realization," Amer. Inst. Chem. Eng. J., vol. 23, p. 135,
- Jan. 1977. [7] M. Lal and R. Mitra, "A comparison of transfer function simplification methods,"
- IEEE Trans. Automat. Contr., vol. AC-19, pp. 627-628, Oct. 1974. M. J. Bosley, H. W. Kropholler, and F. P. Lees, "On the relationship between the [8]
- continued fraction expansion and moments matching methods of model reduction,' Int. J. Contr., vol. 18, pp. 461-473, Sept. 1973. S. C. Chuang, "Application of continued-fraction method for modelling transfer
- [9] functions to give more accurate transient response," Electron. Lett., vol. 6, pp. 861-863, 1970.

## A Note on the Model Reduction Problem

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Abstract - A mixed method of model reduction is proposed; it is based on the differentiation method suggested by Gutman et al. [1] and on the

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